



Fundamentals of Accelerator

2012

Day 3

William A. Barletta

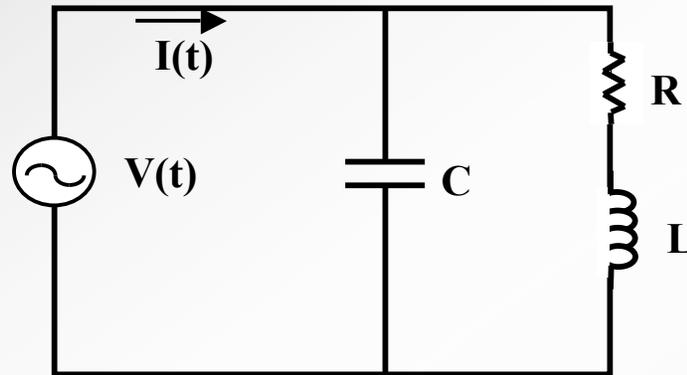
Director, US Particle Accelerator School

Dept. of Physics, MIT

Economics Faculty, University of Ljubljana



Lumped circuit analogy of resonant cavity



$$Z(\omega) = [j\omega C + (j\omega L + R)^{-1}]^{-1}$$

$$Z(\omega) = \frac{1}{j\omega C + (j\omega L + R)^{-1}} = \frac{(j\omega L + R)}{(j\omega L + R)j\omega C + 1} = \frac{(j\omega L + R)}{(1 - \omega^2 LC) + j\omega RC}$$

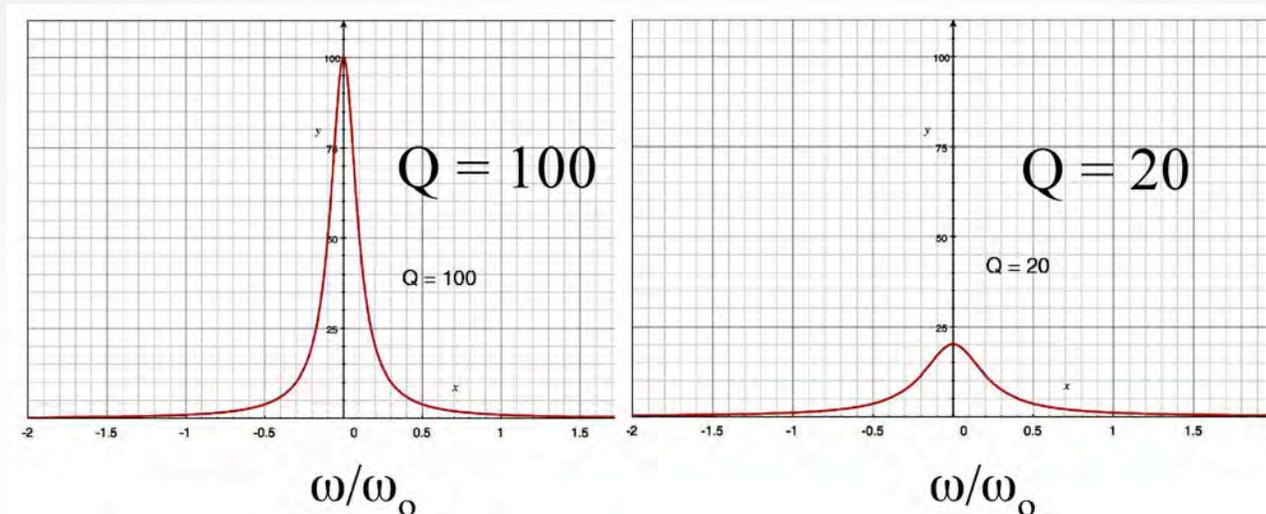
The resonant frequency is $\omega_o = \frac{1}{\sqrt{LC}}$



Q of the lumped circuit analogy

Converting the denominator of Z to a real number we see that

$$|Z(\omega)| \sim \left[\left(1 - \frac{\omega^2}{\omega_0^2} \right)^2 + (\omega RC)^2 \right]^{-1}$$



The width is $\frac{\Delta\omega}{\omega_0} = \frac{R}{\sqrt{L/C}}$



More basics from circuits - Q

$$Q = \frac{\omega_o \circ \text{Energy stored}}{\text{Time average power loss}} = \frac{2\pi \circ \text{Energy stored}}{\text{Energy per cycle}}$$

$$\mathcal{E} = \frac{1}{2} L I_o I_o^* \quad \text{and} \quad \langle \mathcal{P} \rangle = \langle i^2(t) \rangle R = \frac{1}{2} I_o I_o^* R_{\text{surface}}$$

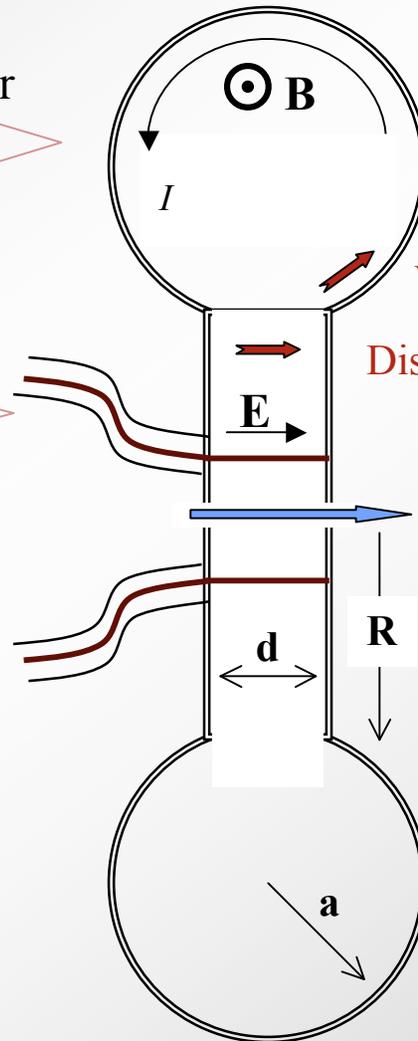
$$\therefore Q = \frac{\sqrt{L/C}}{R} = \left(\frac{\Delta\omega}{\omega_o} \right)^{-1}$$



Translate circuit model to a cavity model: Directly driven, re-entrant RF cavity

Outer region: Large, single turn Inductor

$$L = \frac{\mu_0 \pi a^2}{2\pi(R+a)}$$



*Expanding outer region
raises Q*

Central region: Large plate Capacitor

$$C = \epsilon_0 \frac{\pi R^2}{d}$$



$$\omega_o = \frac{1}{\sqrt{LC}} = c \left[\frac{2((R+a)d)}{\pi R^2 a^2} \right]^{1/2}$$

Wall current

Displacement current

Beam (Load) current

*Narrowing gap
raises shunt impedance*

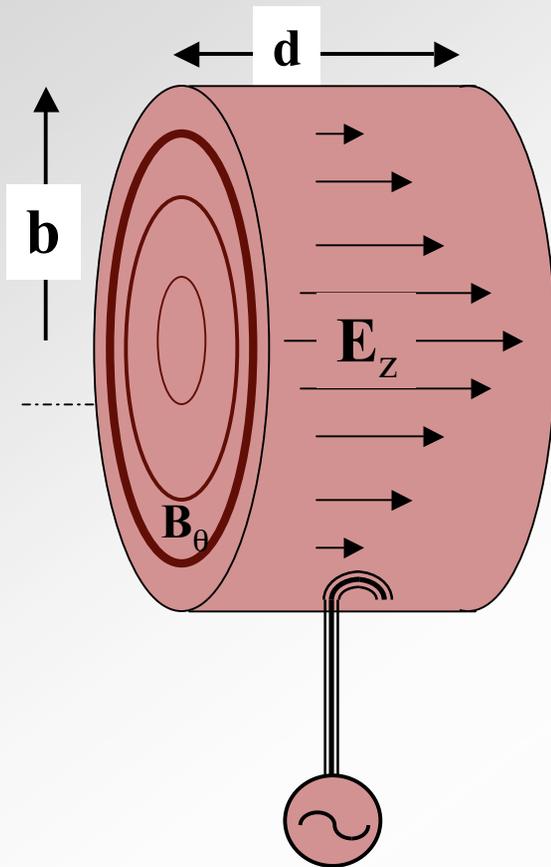
Q – set by resistance in outer region

$$Q = \sqrt{\frac{L}{C}} \frac{1}{R}$$

Source: Humphries, Charged Particle Accelerators



Properties of the RF pillbox cavity



$$\sigma_{walls} = \infty$$

- ❖ We want lowest mode: with only E_z & B_θ
- ❖ Maxwell's equations are:

$$\frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) = \frac{1}{c^2} \frac{\partial}{\partial t} E_z \quad \text{and} \quad \frac{\partial}{\partial r} E_z = \frac{\partial}{\partial t} B_\theta$$

- ❖ Take derivatives

$$\frac{\partial}{\partial t} \left[\frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) \right] = \frac{\partial}{\partial t} \left[\frac{\partial B_\theta}{\partial r} + \frac{B_\theta}{r} \right] = \frac{1}{c^2} \frac{\partial^2 E_z}{\partial t^2}$$

$$\frac{\partial}{\partial r} \frac{\partial E_z}{\partial r} = \frac{\partial}{\partial r} \frac{\partial B_\theta}{\partial t}$$

\implies

$$\frac{\partial^2 E_z}{\partial r^2} + \frac{1}{r} \frac{\partial E_z}{\partial r} = \frac{1}{c^2} \frac{\partial^2 E_z}{\partial t^2}$$



For a mode with frequency ω

- ❖
$$E_z(r, t) = E_z(r) e^{i\omega t}$$
- ❖ Therefore,
$$E_z'' + \frac{E_z'}{r} + \left(\frac{\omega}{c}\right)^2 E_z = 0$$
 - (Bessel's equation, 0 order)

❖ Hence,

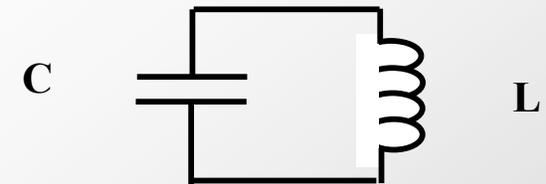
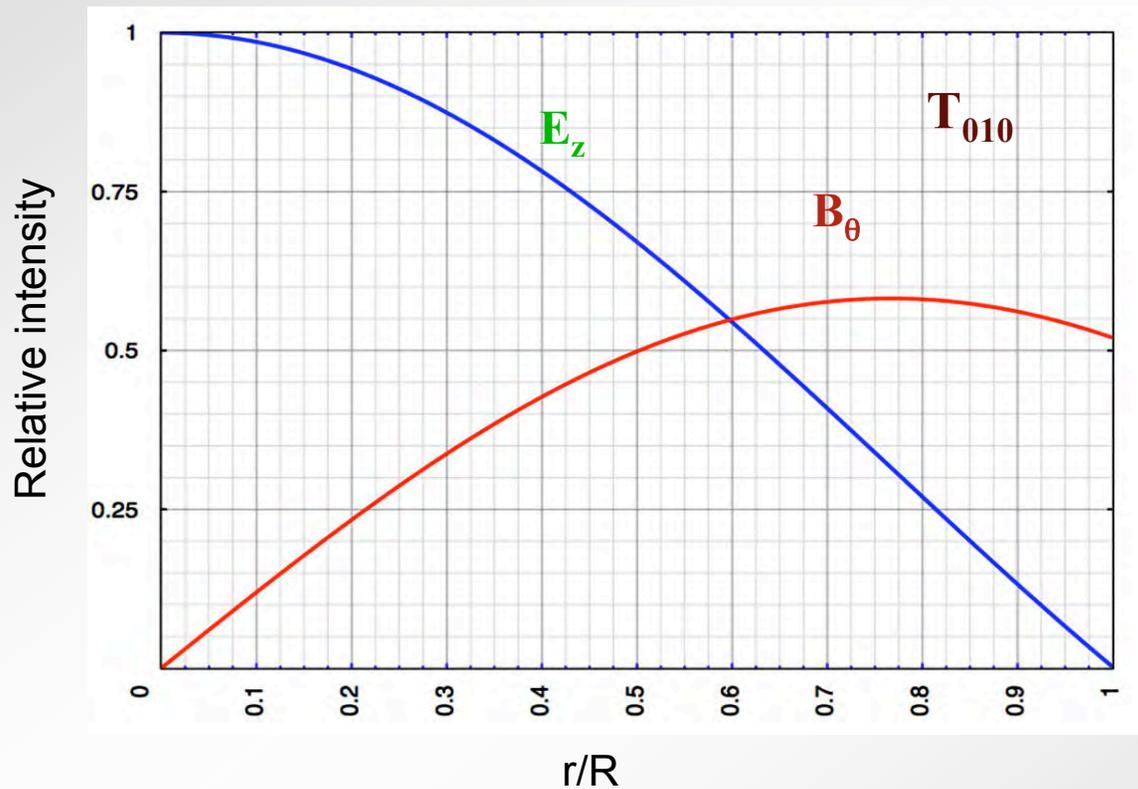
$$E_z(r) = E_o J_0\left(\frac{\omega}{c} r\right)$$

❖ For conducting walls, $E_z(R) = 0$, therefore

$$\frac{2\pi f}{c} b = 2.405$$

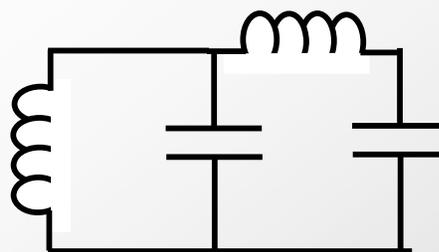
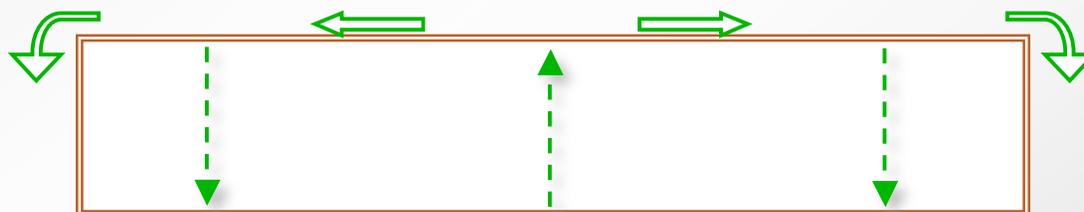
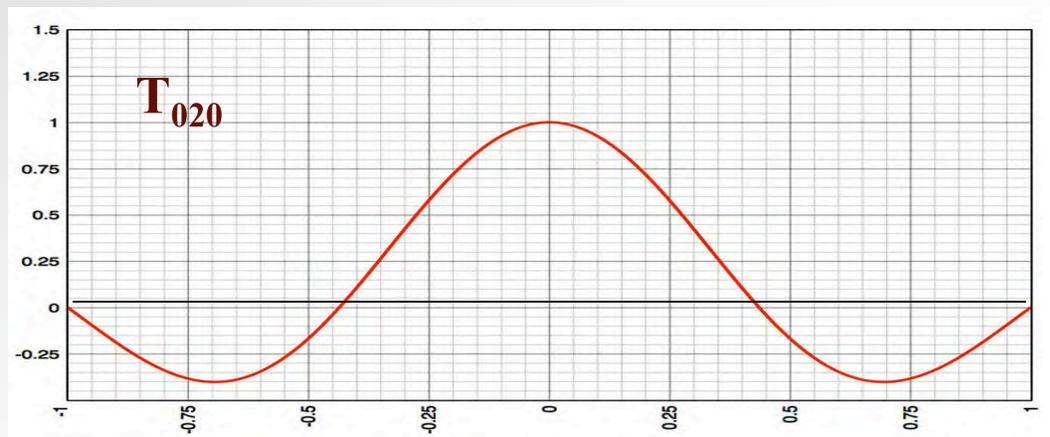


E-fields & equivalent circuit: T_{0n10} mode



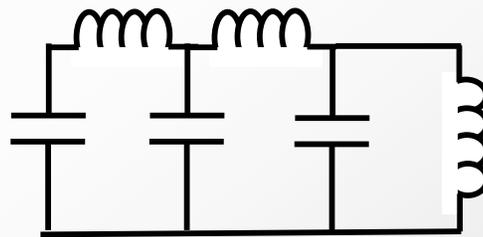
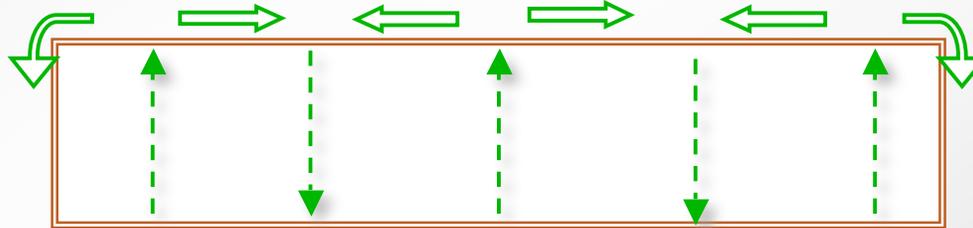
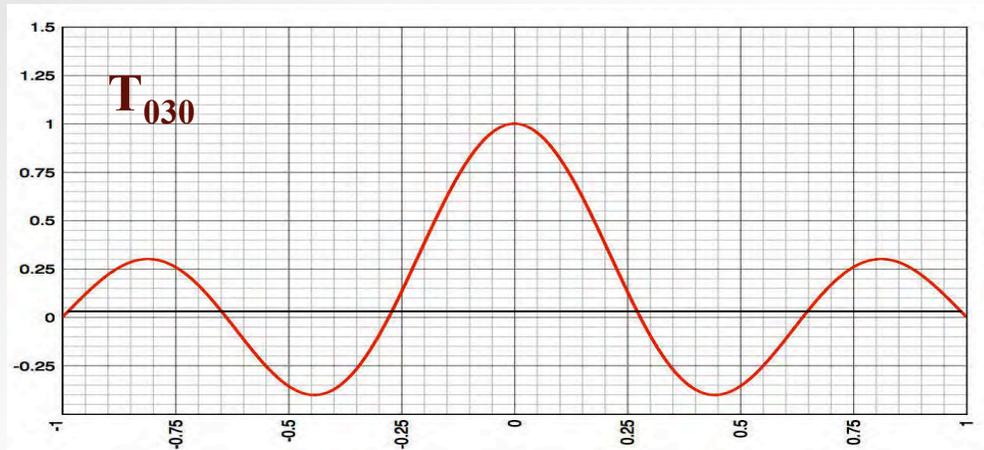


E-fields & equivalent circuits for T_{020} modes





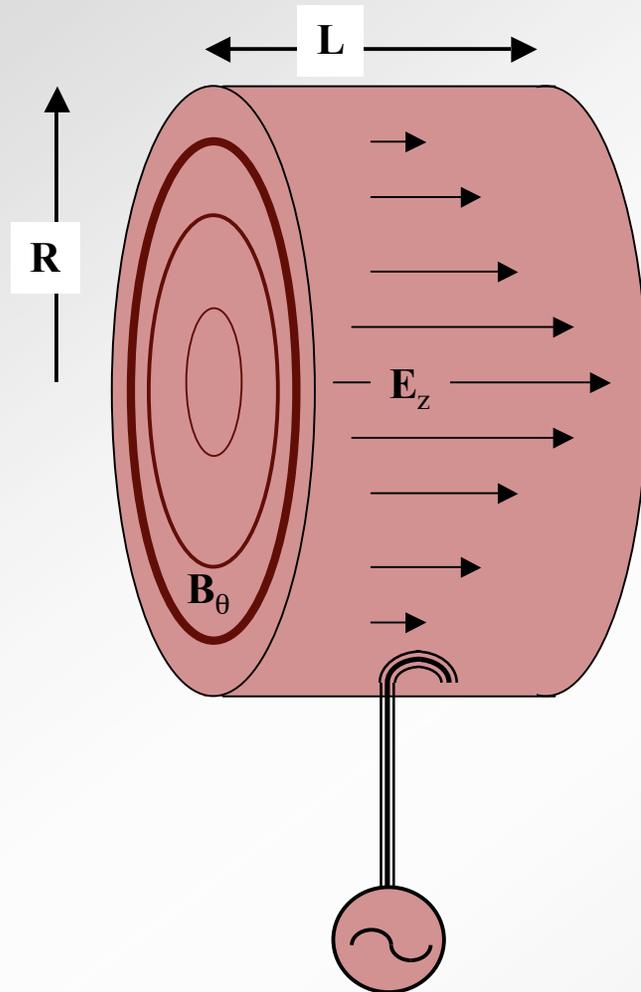
E-fields & equivalent circuits for T_{on0} modes



T_{on0} has
 n coupled, resonant
circuits; each L & C
reduced by $1/n$



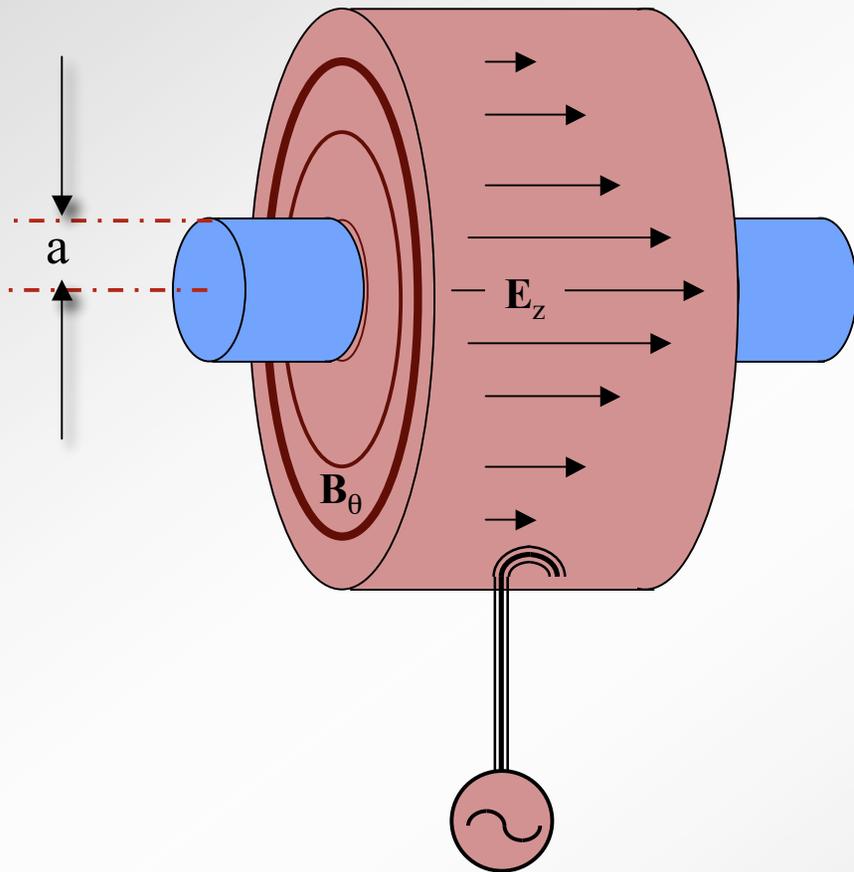
Simple consequences of pillbox model



- ❖ Increasing R lowers frequency
==> Stored Energy, $\mathcal{E} \sim \omega^{-2}$
- ❖ $\mathcal{E} \sim E_z^2$
- ❖ Beam loading lowers E_z for the next bunch
- ❖ Lowering ω lowers the fractional beam loading
- ❖ Raising ω lowers $Q \sim \omega^{-1/2}$
- ❖ If time between beam pulses,
 $T_s \sim Q/\omega$
almost all \mathcal{E} is lost in the walls



The beam tube makes field modes (& cell design) more complicated



- ❖ Peak E no longer on axis
 - $E_{pk} \sim 2 - 3 \times E_{acc}$
 - $FOM = E_{pk}/E_{acc}$
- ❖ ω_0 more sensitive to cavity dimensions
 - Mechanical tuning & detuning
- ❖ Beam tubes add length & ϵ 's w/o acceleration
- ❖ Beam induced voltages $\sim a^{-3}$
 - Instabilities

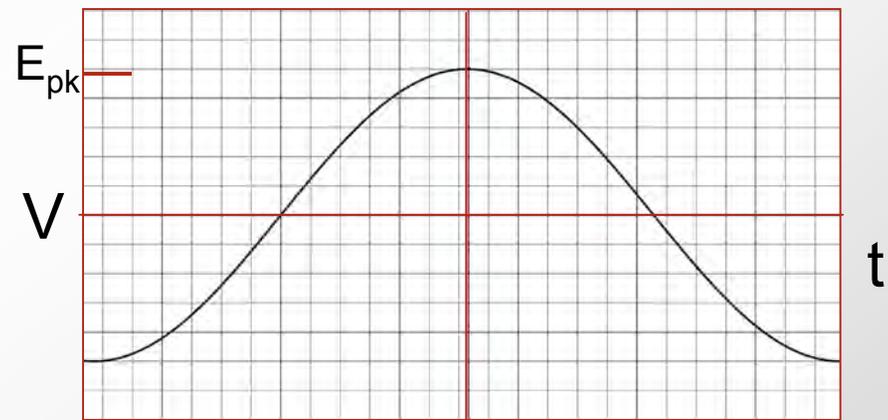
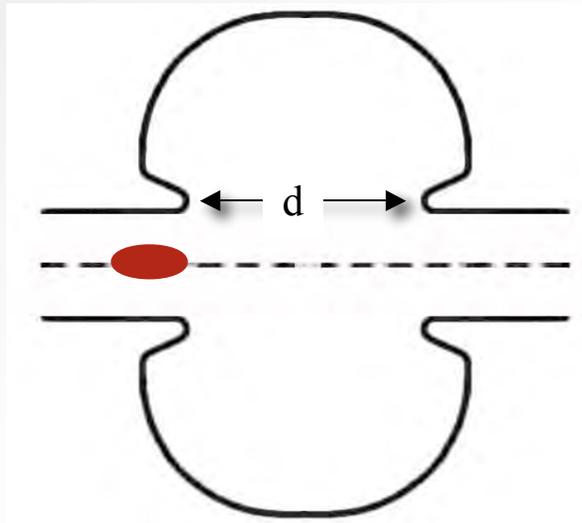
Cavity figures of merit



Figure of Merit: Accelerating voltage

- ❖ The voltage varies during time that bunch takes to cross gap
 - reduction of the peak voltage by Γ (transt time factor)

$$\Gamma = \frac{\sin(\vartheta/2)}{\vartheta/2} \quad \text{where } \vartheta = \omega d / \beta c$$



For maximum acceleration

$$T_{\text{cav}} = \frac{d}{c} = \frac{T_{\text{rf}}}{2} \implies \Gamma = 2/\pi$$



Figure of merit from circuits - Q

$$Q = \frac{\omega_o \circ \text{Energy stored}}{\text{Time average power loss}} = \frac{2\pi \circ \text{Energy stored}}{\text{Energy lost per cycle}}$$

$$\mathcal{E} = \frac{\mu_o}{2} \int_v |H|^2 dv = \frac{1}{2} L I_o I_o^*$$

$$\langle \mathcal{P} \rangle = \frac{R_{surf}}{2} \int_s |H|^2 ds = \frac{1}{2} I_o I_o^* R_{surf}$$

$$R_{surf} = \frac{1}{\text{Conductivity} \circ \text{Skin depth}} \sim \omega^{1/2}$$

$$\therefore Q = \frac{\sqrt{L/C}}{R_{surf}} = \left(\frac{\Delta\omega}{\omega_o} \right)^{-1}$$



Measuring the energy stored in the cavity allows us to measure Q

- ❖ We have computed the field in the fundamental mode

$$\begin{aligned} U &= \int_0^d dz \int_0^b dr 2\pi r \left(\frac{\epsilon E_o^2}{2} \right) J_1^2(2.405r/b) \\ &= b^2 d \left(\epsilon E_o^2 / 2 \right) J_1^2(2.405) \end{aligned}$$

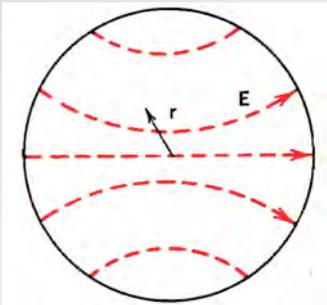
- ❖ To measure Q we excite the cavity and measure the E field as a function of time
- ❖ Energy lost per half cycle = $U\pi Q$
- ❖ Note: energy can be stored in the higher order modes that deflect the beam



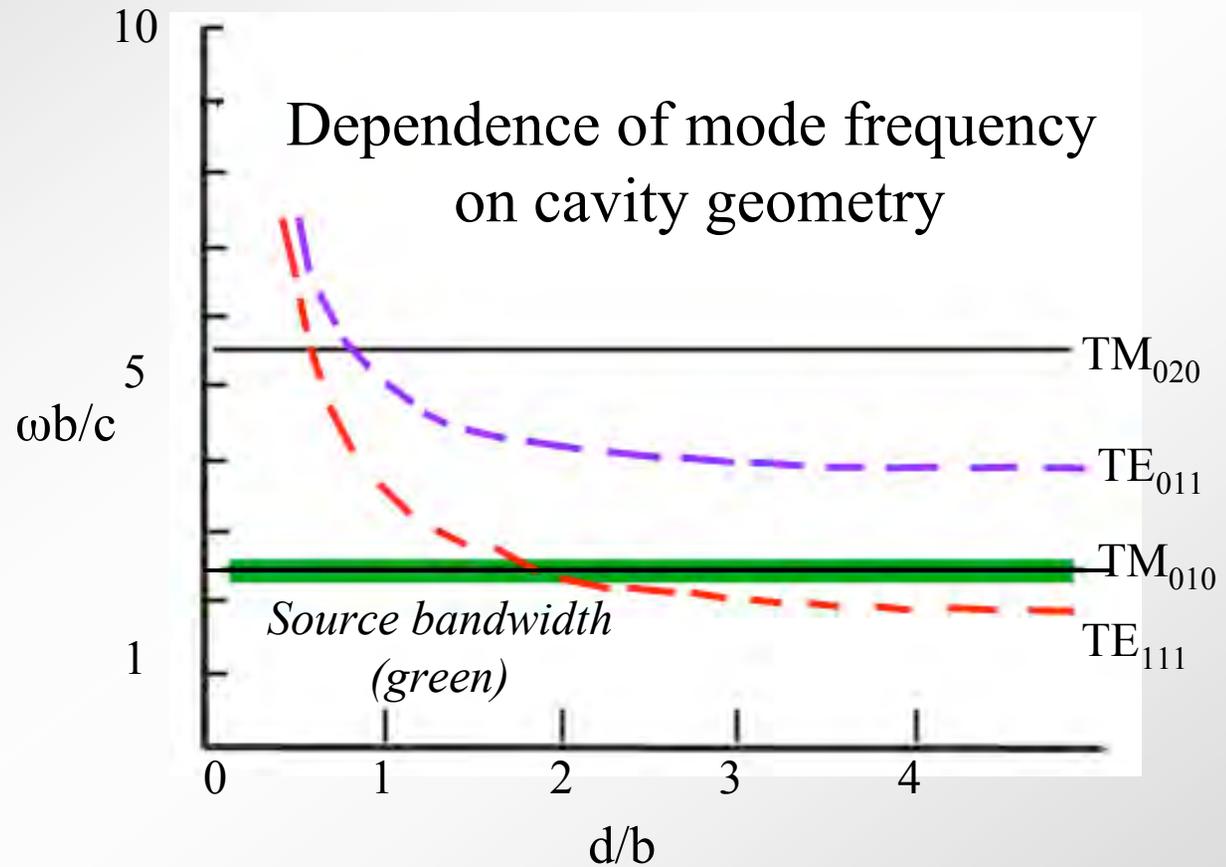
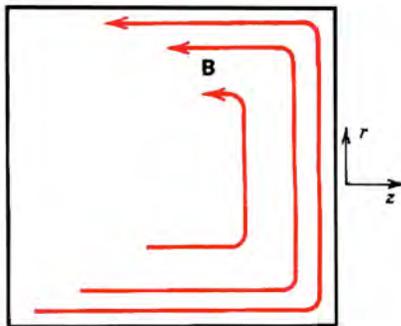
Keeping energy out of higher order modes

TE₁₁₁ mode

End view



Side view



Choose cavity dimensions to stay far from crossovers



Figure of merit for accelerating cavity: Power to produce the accelerating field

Resistive input (shunt) impedance at ω_0 relates power dissipated in walls to accelerating voltage

$$R_{in} = \frac{\langle V^2(t) \rangle}{\mathcal{P}} = \frac{V_o^2}{2\mathcal{P}} = Q\sqrt{L/C}$$

Linac literature commonly defines “shunt impedance” without the “2”

$$\mathcal{R}_{in} = \frac{V_o^2}{\mathcal{P}} \sim \frac{1}{R_{surf}}$$

Typical values 25 - 50 M Ω



Computing shunt impedance

$$R_{in} = \frac{V_o^2}{\mathcal{P}}$$

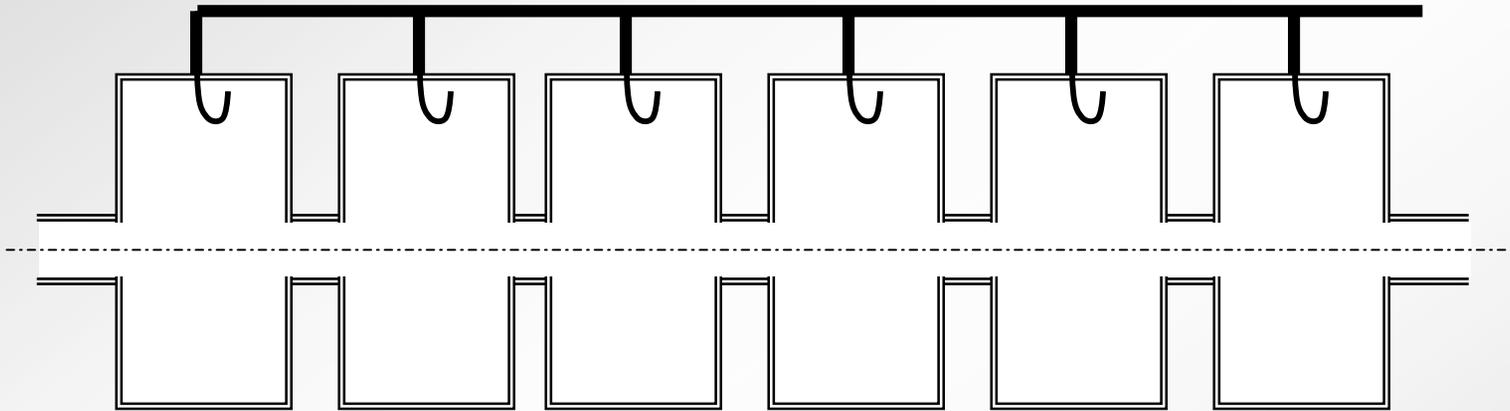
$$\langle \mathcal{P} \rangle = \frac{R_{surf}}{2} \int_s |H|^2 ds$$

$$R_{surf} = \frac{\mu\omega}{2\sigma_{dc}} = \pi Z_o \frac{\delta_{skin}}{\lambda_{rf}} \quad \text{where } Z_o = \sqrt{\frac{\mu_o}{\epsilon_o}} = 377\Omega$$

The on-axis field E and surface H are generally computed with a computer code such as SUPERFISH for a complicated cavity shape



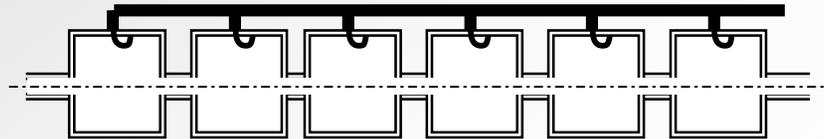
To make a linac Use a series of pillbox cavities



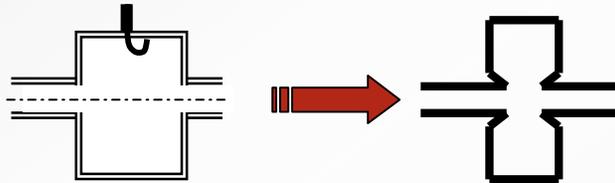
Power the cavities so that $E_z(z,t) = E_z(z)e^{i\omega t}$



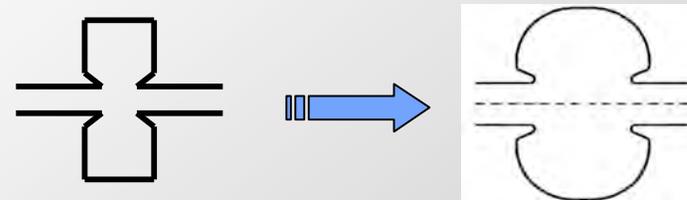
Improve on the array of pillboxes?



- ❖ Return to the picture of the re-entrant cavity

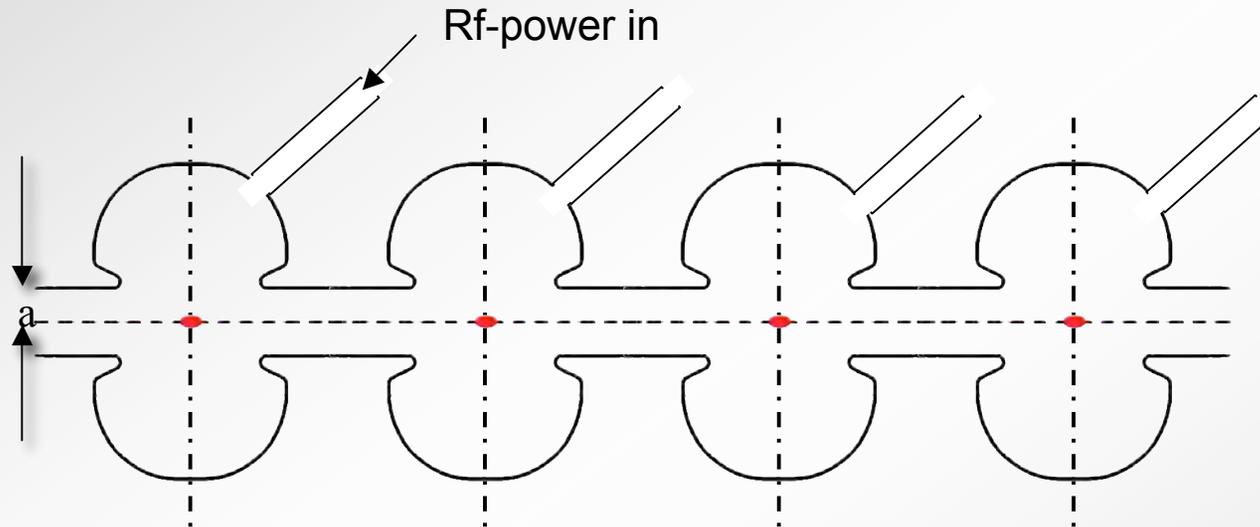


- ❖ Nose cones concentrate E_z near beam for fixed stored energy
- ❖ Optimize nose cone to maximize V^2 ; I.e., maximize R_{sh}/Q
- ❖ Make H-field region nearly spherical; raises Q & minimizes P for given stored energy





Thus, linacs can be considered to be an array of distorted pillbox cavities...



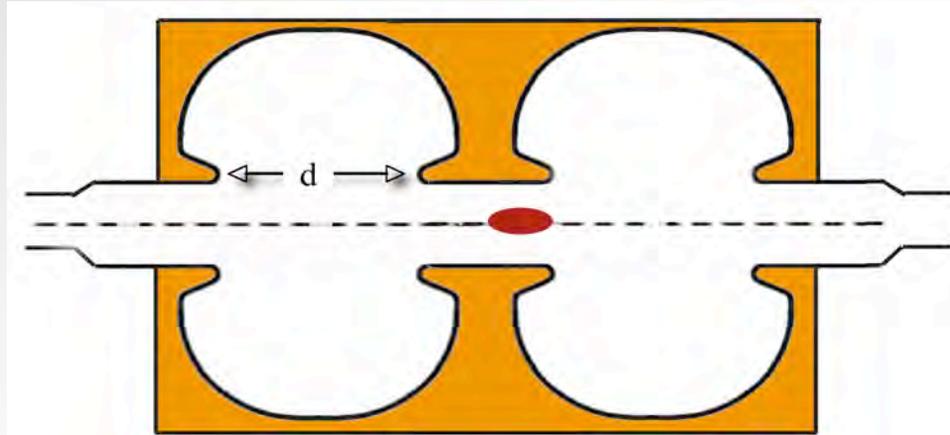
In warm linacs “nose cones” optimize the voltage per cell with respect to resistive dissipation

$$Q = \sqrt{L/C} / \mathcal{R}_{\text{surface}}$$

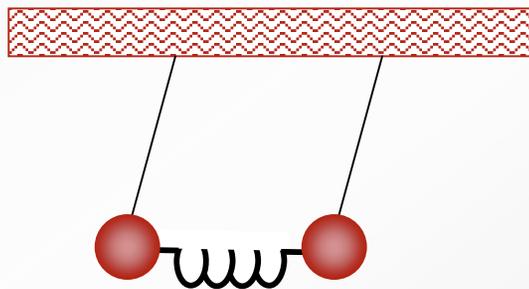
Usually cells are feed in groups not individually.... and



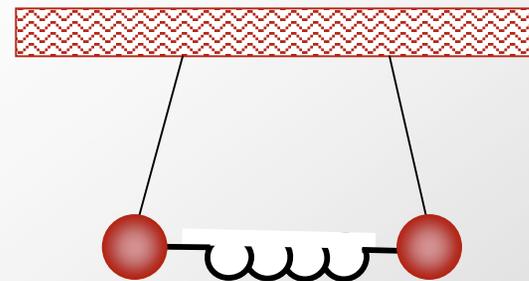
Linacs cells are linked to minimize cost



==> coupled oscillators ==> multiple modes



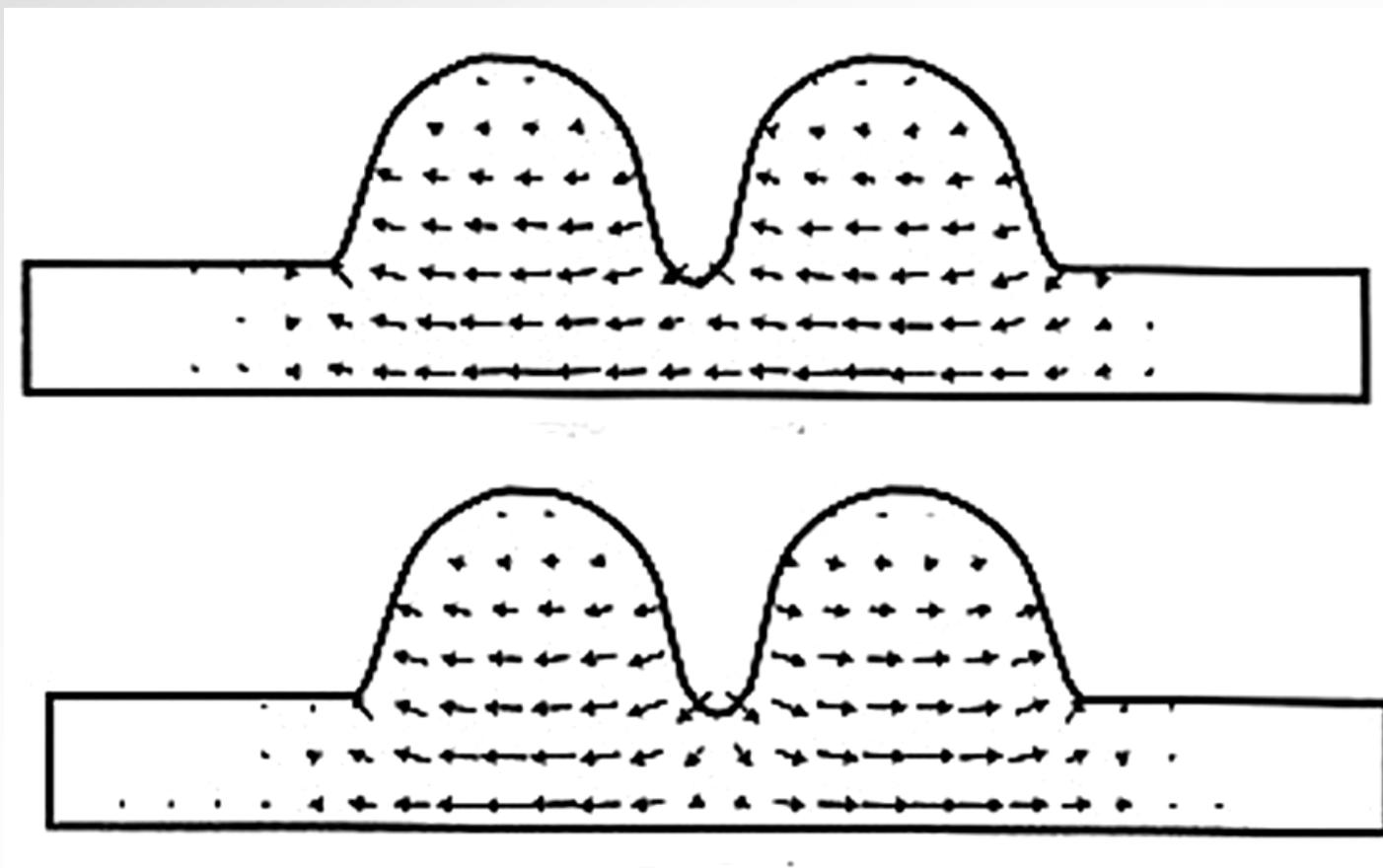
Zero mode



π mode

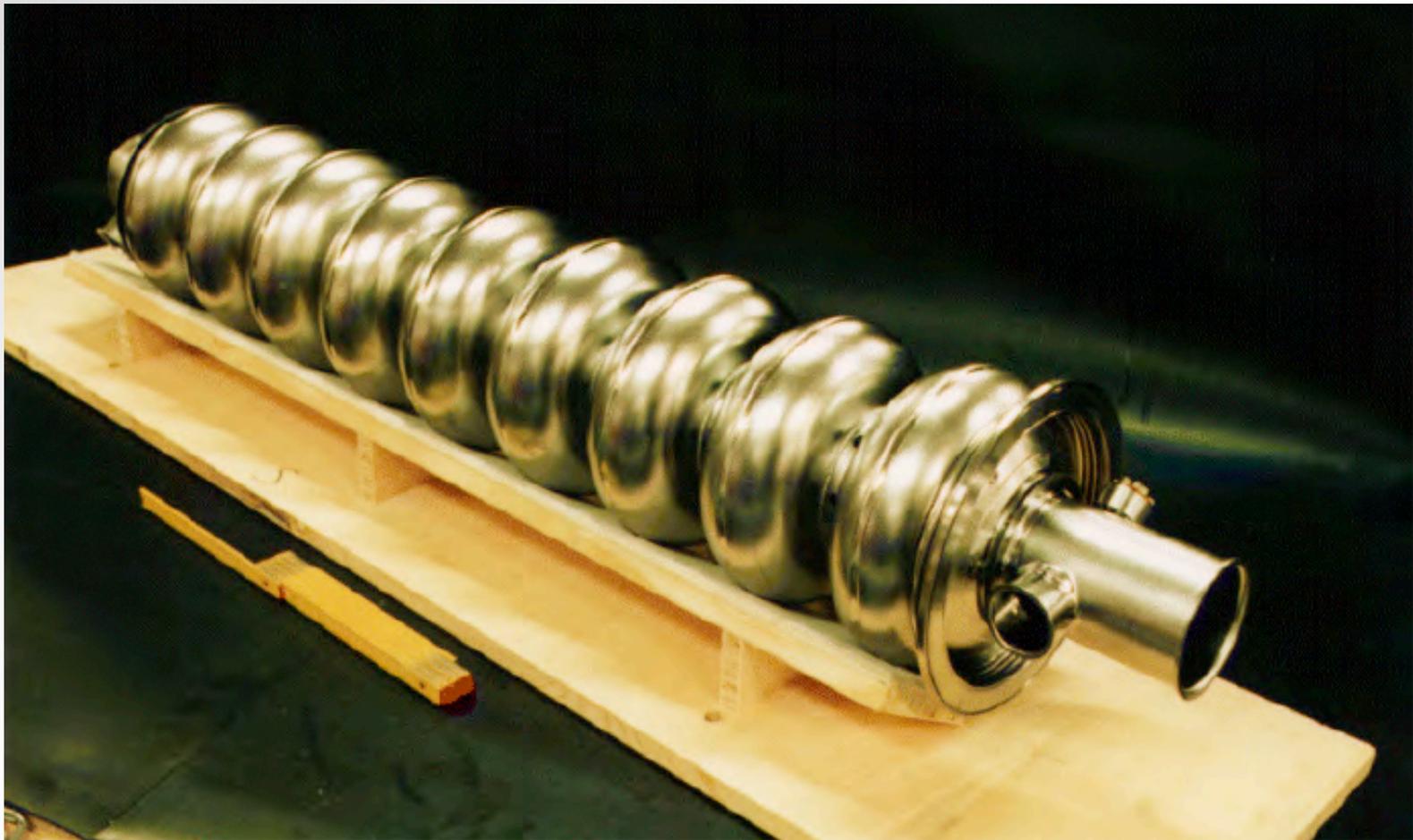


Modes of a two-cell cavity



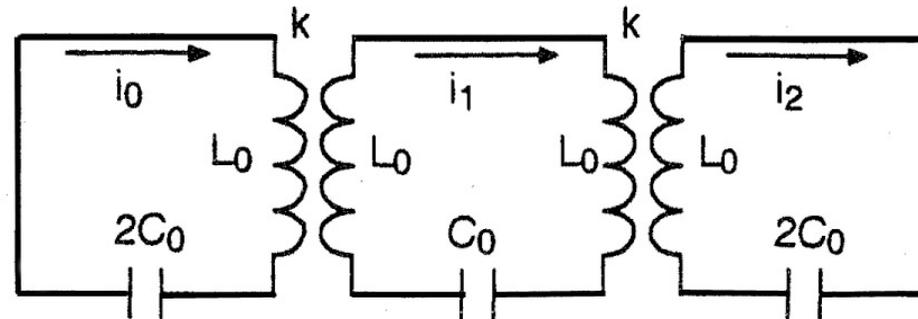


9-cavity TESLA cell





Example of 3 coupled cavities



$$x_0 \left(1 - \frac{\omega_0^2}{\Omega^2} \right) + x_1 k = 0 \quad \text{oscillator } n = 0$$

$$x_1 \left(1 - \frac{\omega_0^2}{\Omega^2} \right) + (x_0 + x_2) \frac{k}{2} = 0 \quad \text{oscillator } n = 1$$

$$x_2 \left(1 - \frac{\omega_0^2}{\Omega^2} \right) + x_1 k = 0 \quad \text{oscillator } n = 2$$

$$x_j = i_j \sqrt{2L_0} \quad \text{and} \quad \Omega = \text{normal mode frequency}$$



Write the coupled circuit equations in matrix form

$$\mathbf{L}\mathbf{x}_q = \frac{1}{\Omega_q^2} \mathbf{x}_q \quad \text{where} \quad \mathbf{L} = \begin{pmatrix} 1/\omega_o^2 & k/\omega_o^2 & 0 \\ k/2\omega_o^2 & 1/\omega_o^2 & k/2\omega_o^2 \\ 0 & k/\omega_o^2 & 1/\omega_o^2 \end{pmatrix} \quad \text{and} \quad \mathbf{x}_q = \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$$

- ❖ Compute eigenvalues & eigenvectors to find the three normal modes

$$\text{Mode } q=0: \text{ zero mode} \quad \Omega_0 = \frac{\omega_o}{\sqrt{1+k}} \quad \mathbf{x}_0 = \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

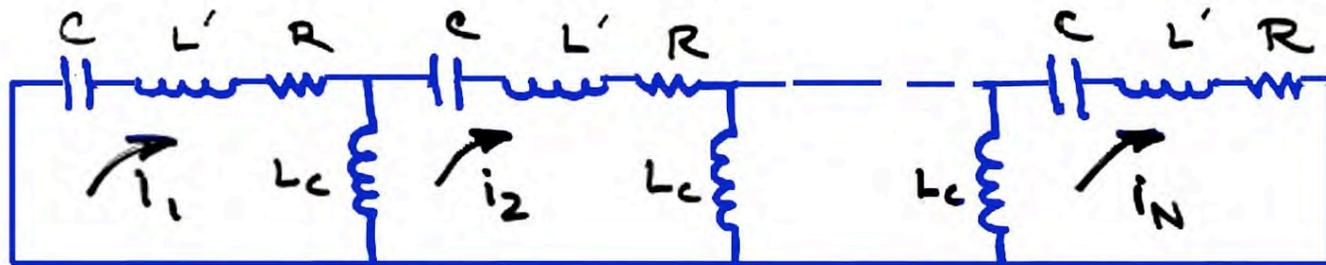
$$\text{Mode } q=1: \pi/2 \text{ mode} \quad \Omega_1 = \omega_o \quad \mathbf{x}_1 = \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix}$$

$$\text{Mode } q=2: \pi \text{ mode} \quad \Omega_2 = \frac{\omega_o}{\sqrt{1-k}} \quad \mathbf{x}_2 = \begin{pmatrix} 1 \\ -1 \\ 1 \end{pmatrix}$$



For a structure with N coupled cavities

- ❖ \implies Set of N coupled oscillators
 - N normal modes, N frequencies
- ❖ From the equivalent circuit with magnetic coupling



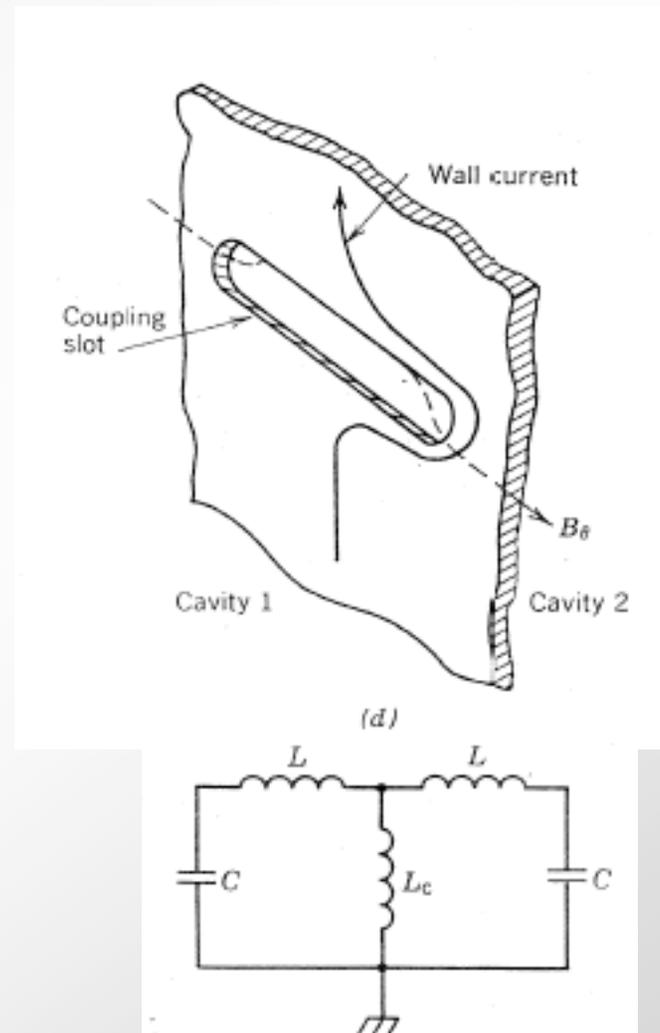
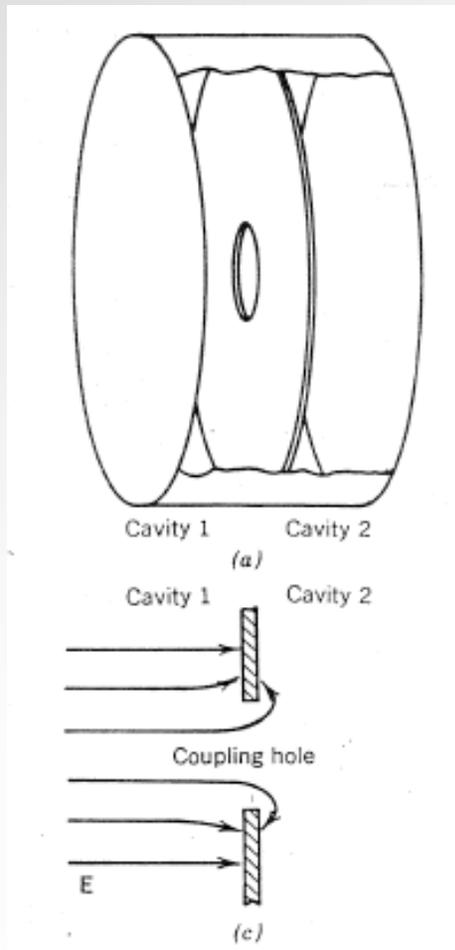
$$\omega_m = \frac{\omega_o}{\left(1 - B \cos \frac{m\pi}{N}\right)^{1/2}} \approx \omega_o \left(1 + B \cos \frac{m\pi}{N}\right)$$

where B = bandwidth (frequency difference between lowest & high frequency mode)

- ❖ Typically accelerators run in the π -mode

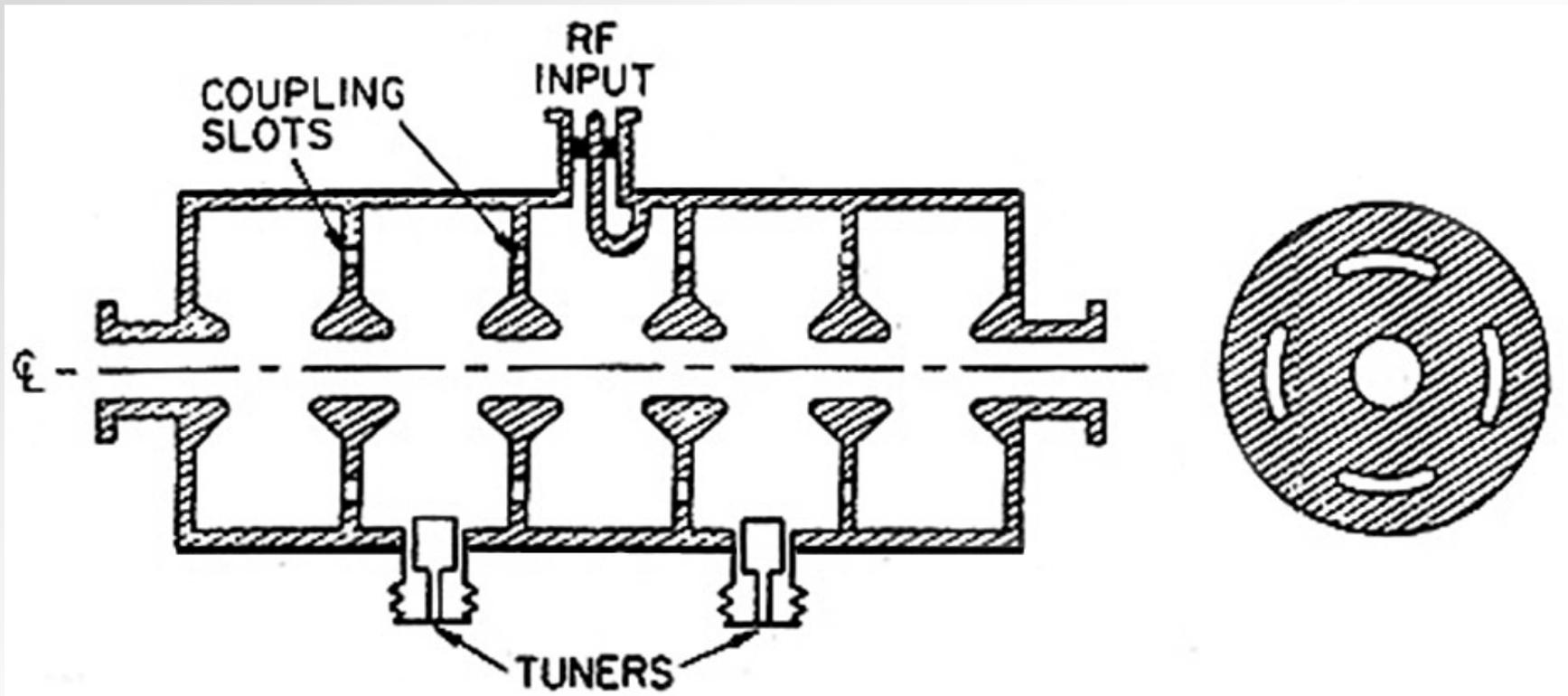


Magnetically coupled pillbox cavities





5-cell π -mode cell with magnetic coupling

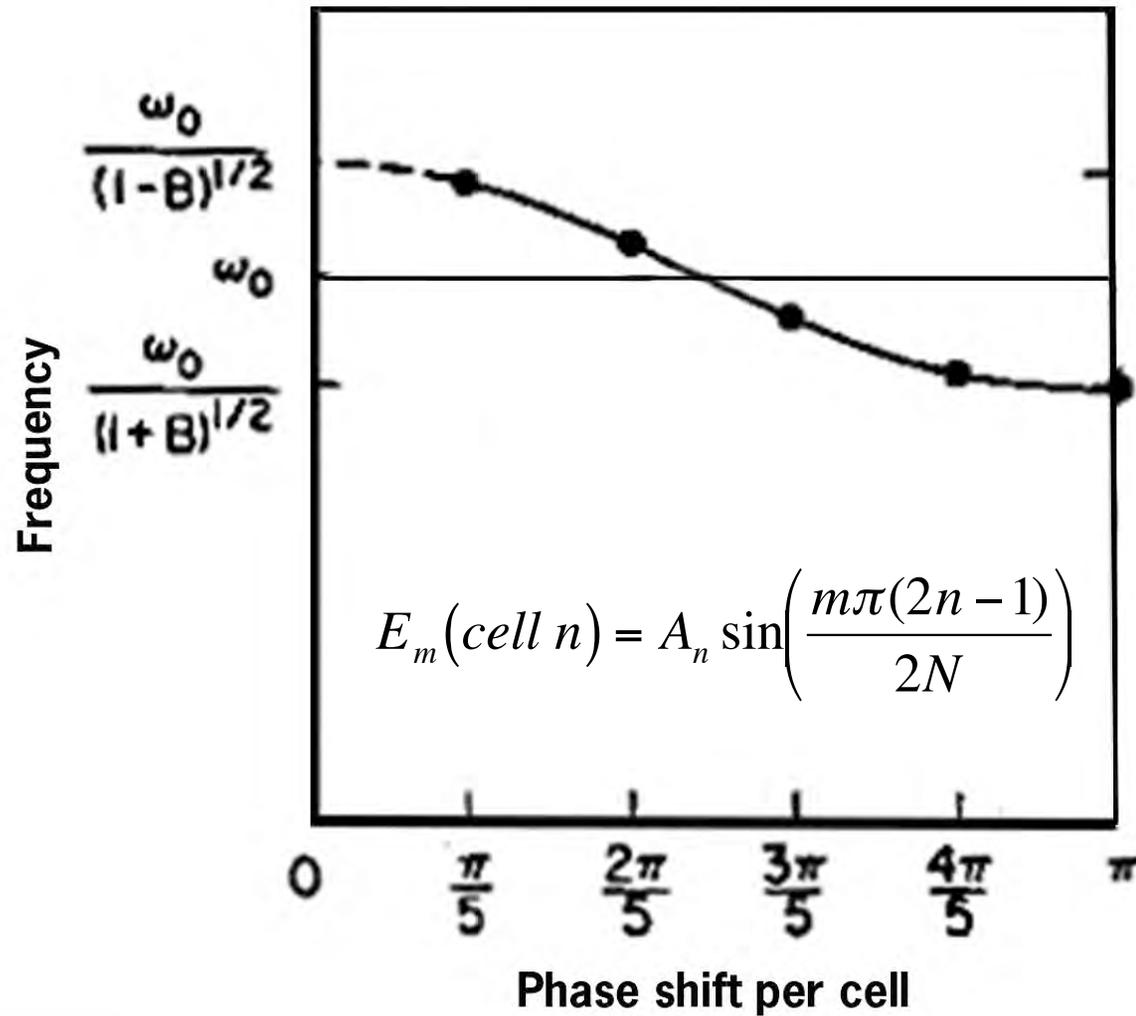


The tuners change the frequencies by perturbing wall currents \implies changes the inductance \implies changes the energy stored in the magnetic field

$$\frac{\Delta\omega_o}{\omega_o} = \frac{\Delta U}{U}$$

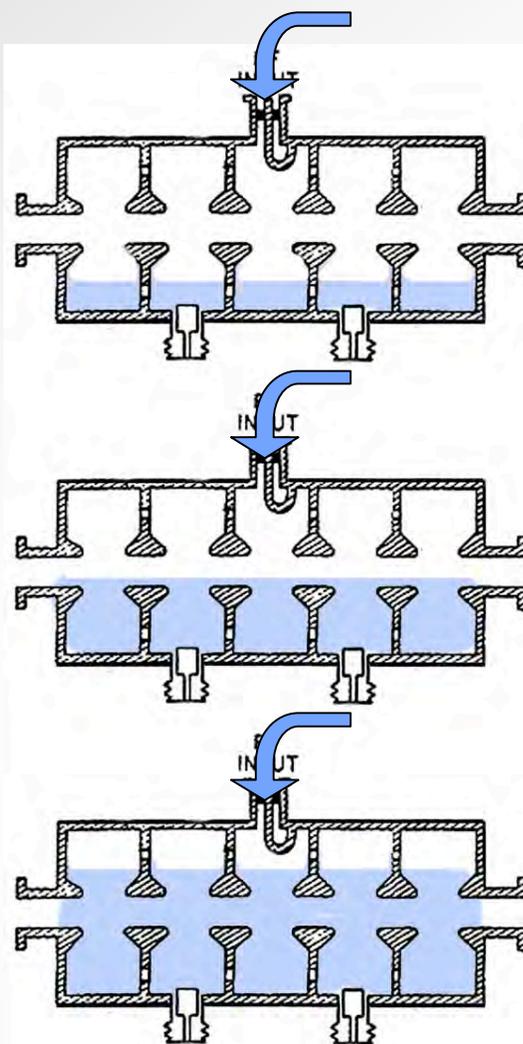


Dispersion diagram for 5-cell structure





Schematic of energy flow in a standing wave structure



What makes SC RF attractive?



Comparison of SC and NC RF

Superconducting RF

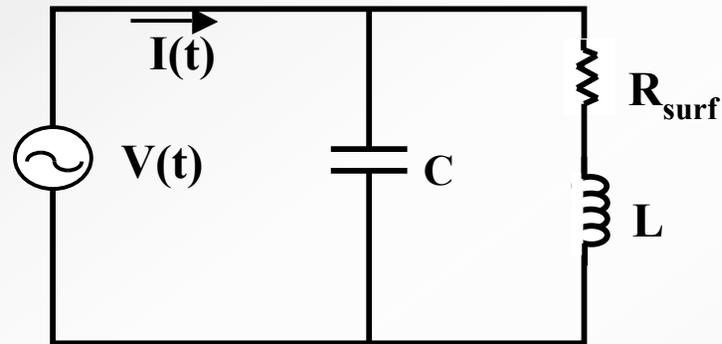
- ❖ High gradient
==> 1 GHz, meticulous care
- ❖ Mid-frequencies
==> Large stored energy, \mathcal{E}_s
- ❖ Large \mathcal{E}_s
==> very small $\Delta E/E$
- ❖ Large Q
==> high efficiency

Normal Conductivity RF

- ❖ High gradient
==> high frequency (5 - 17 GHz)
- ❖ High frequency
==> low stored energy
- ❖ Low \mathcal{E}_s
==> $\sim 10x$ larger $\Delta E/E$
- ❖ Low Q
==> reduced efficiency



Recall the circuit analog



As $R_{surf} \implies 0$, the $Q \implies \infty$.

In practice,

$$Q_{nc} \sim 10^4$$

$$Q_{sc} \sim 10^{11}$$



Figure of merit for accelerating cavity: power to produce the accelerating field

Resistive input (shunt) impedance at ω_0 relates power dissipated in walls to accelerating voltage

$$R_{in} = \frac{\langle V^2(t) \rangle}{\mathcal{P}} = \frac{V_o^2}{2\mathcal{P}} = Q\sqrt{L/C}$$

Linac literature more commonly defines “shunt impedance” without the “2”

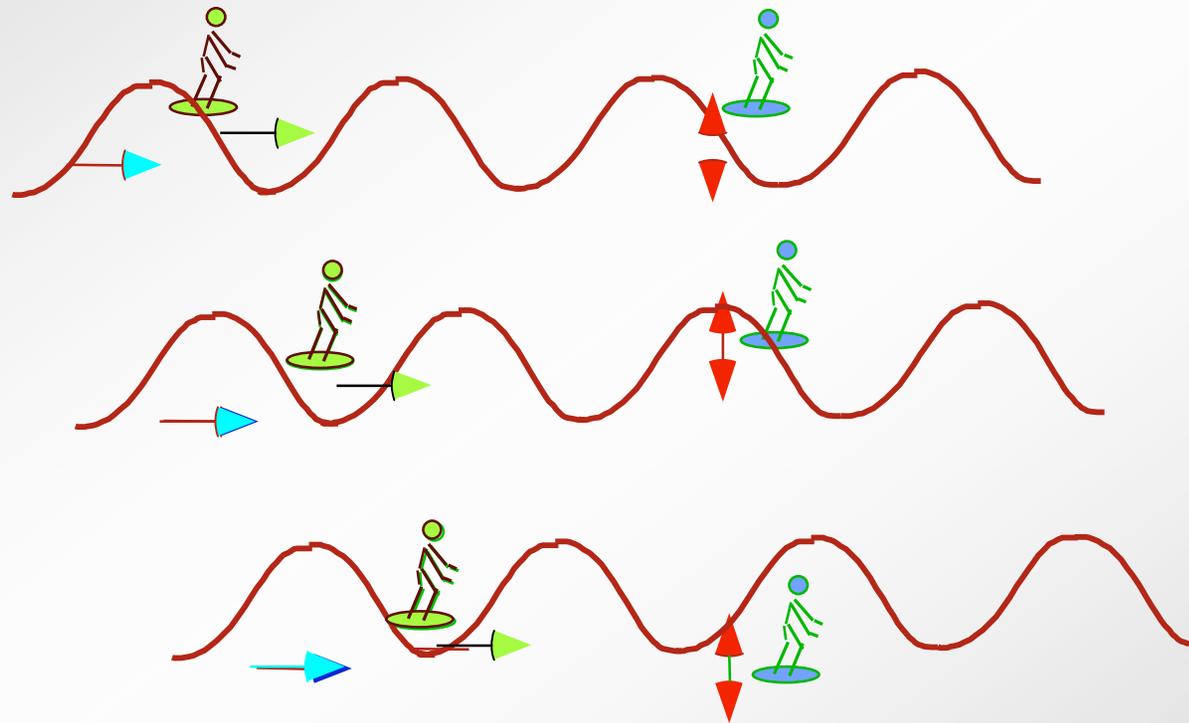
$$\mathcal{R}_{in} = \frac{V_o^2}{\mathcal{P}} \sim \frac{1}{R_{surf}}$$

For SC-rf \mathcal{P} is reduced by orders of magnitude

BUT, it is deposited @ 2K



Surfing analogy of the traveling wave acceleration mechanism

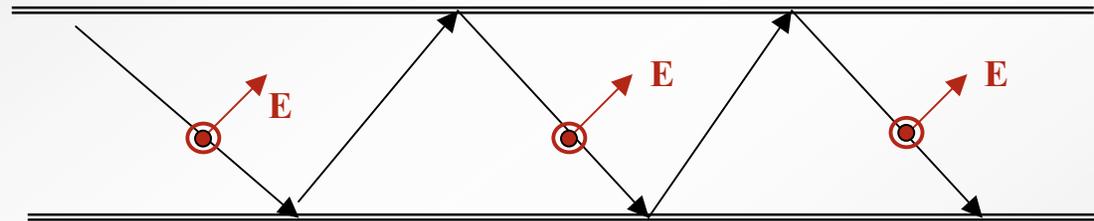


To “catch” the wave the surfer must be synchronous with the phase velocity of the wave



Typically we need a longitudinal E-field to accelerate particles in vacuum

- ❖ Example: the standing wave structure in a pillbox cavity
- ❖ What about traveling waves?
 - Waves guided by perfectly conducting walls can have E_{long}



- ❖ But first, think back to phase stability
 - To get continual acceleration the wave & the particle must stay in phase
 - Therefore, we can accelerate a charge with a wave with a synchronous phase velocity, $v_{\text{ph}} \approx v_{\text{particle}} < c$



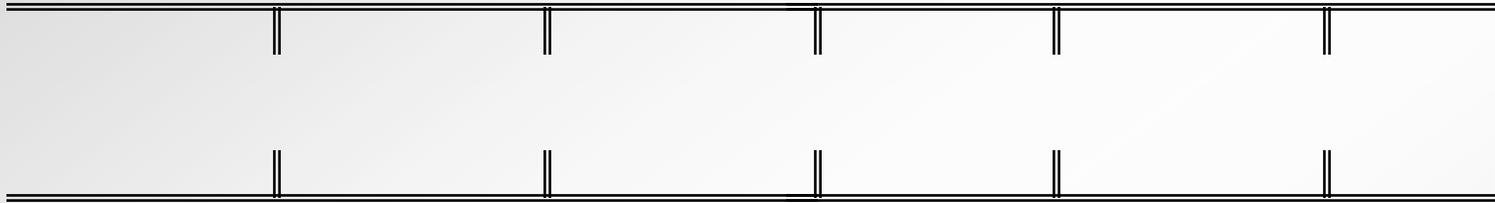
Can the accelerating structure be a simple (smooth) waveguide?

- ❖ Assume the answer is “yes”
- ❖ Then $\mathbf{E} = \mathbf{E}(r, \theta) e^{i(\omega t - kz)}$ with $\omega/k = v_{ph} < c$
- ❖ Transform to the frame co-moving at $v_{ph} < c$
- ❖ Then,
 - The structure is unchanged (by hypothesis)
 - \mathbf{E} is static (v_{ph} is zero in this frame)
 - ==> By Maxwell's equations, $\mathbf{H} = 0$
 - ==> $\nabla \circ \mathbf{E} = 0$ and $\mathbf{E} = -\nabla \phi$
 - But ϕ is constant at the walls (metallic boundary conditions)
 - ==> $\mathbf{E} = 0$

The assumption is false, smooth structures have $v_{ph} > c$



To slow the wave, add irises



In a transmission line the irises

- a) Increase capacitance, C
- b) Leave inductance \sim constant
- c) \implies lower impedance, Z
- d) \implies lower v_{ph}

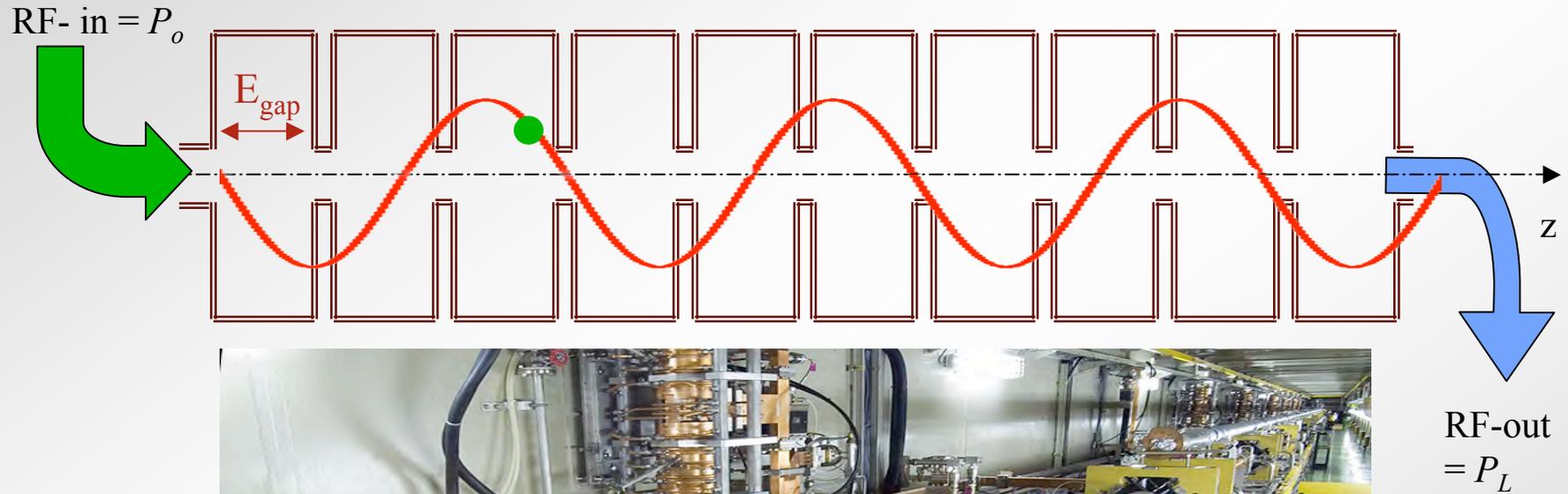
$$\frac{\omega}{k} = \frac{1}{\sqrt{LC}}$$

$$Z = \frac{L}{C}$$

Similar for TM₀₁ mode in the waveguide



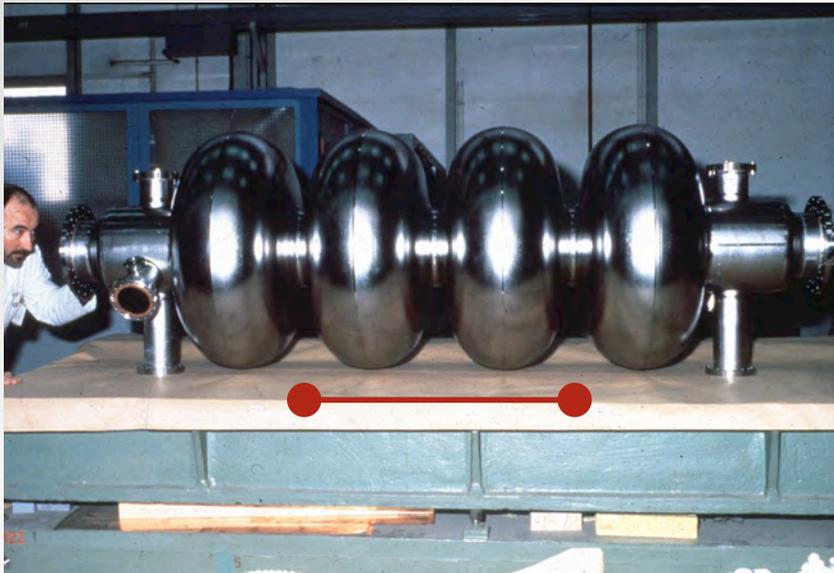
Ultra-relativistic particles ($v \approx c$) can “surf” an rf field traveling at c





RF-cavities in metal and in plasma

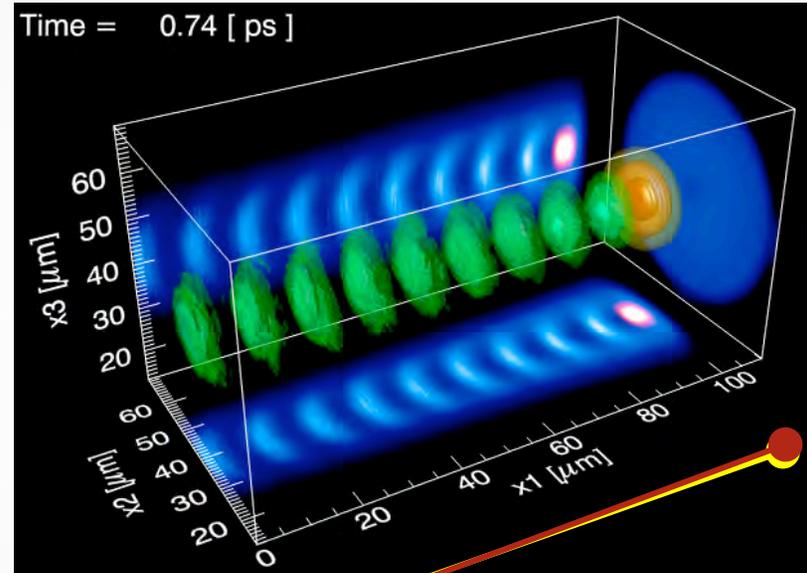
Think back to the string of pillboxes



1 m
RF cavity

$G \sim 30 \text{ MeV/m}$

Courtesy of W. Mori & L. da Silva



100 μm
Plasma cavity

$G \sim 30 \text{ GeV/m}$

End of unit